

ON THE METHOD FOR THE SOLUTION OF ONE PROBLEM OF THE ELASTICITY THEORY

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ABSTRACT

This paper is devoted to a method of obtaining the equation describing the bend of the round fixed plate under the loading, concentrated at the point and on the interior circumference.

Key words: bend of the round fixed plate, Gilbert boundary value problem

1. THE SOLUTION OF THE GILBERT BOUNDARY VALUE PROBLEM FOR ROUND REGION

Let us consider the following problem. It is required to find all real valued byharmonic in T^+ functions $U(x, y)$, continuous in $T^+ \cup L$ with their partial derivatives of the first order and satisfying on L the following conditions:

$$\frac{\partial U}{\partial x} = c_1(t), \quad \frac{\partial U}{\partial y} = c_2(t), \quad (1.1)$$

where $c_1(t)$, $c_2(t)$ are given real-valued functions, belonging to the class $H^1(L)$.

The problem (1.1) is a special case of the so-called Gilbert-type boundary value problem for byanalytic functions

$$\begin{cases} a_1(t) \frac{\partial u}{\partial x} + b_1(t) \frac{\partial v}{\partial x} = c_1(t), \\ a_2(t) \frac{\partial u}{\partial y} + b_2(t) \frac{\partial v}{\partial y} = c_2(t), \end{cases} \quad (1.2)$$

where $a_k(t)$, $b_k(t)$, $c_k(t)$ ($k = 1, 2$) are given real valued functions of the complex argument, satisfying on L the Holder condition with their derivatives

up to the order $(3 - k)$, and $[a_k(t)]^2 + [b_k(t)]^2 = 1$. So, we can obtain the solution of the problem (1.1) from formulae for (1.2). As an example, let us obtain the solution of problem (1.1) for the round regions.

The solution of problem (1.2) is being searched in the form

$$F(z) = \varphi_0(z) + \bar{z}\varphi_1(z),$$

where $\phi_0(z)$, $\phi_1(z)$ are analytic functions in the circle K_1 . Then the solution of problem (1.1) can be obtained by the formula

$$U(x, y) = \operatorname{Re}[\varphi_0(z) + \bar{z}\varphi_1(z)].$$

We see, that the values of imaginary parts of $\phi_0(z)$ and $\bar{z}\phi_1(z)$ do not influence the solution of problem (1.1). So without the restriction on generality we can suppose, that the following initial conditions are fulfilled:

$$\operatorname{Im}\varphi_0(0) = 0, \quad \varphi_1(0), \quad \operatorname{Im}\varphi_1' = 0. \quad (1.3)$$

Then we can rewrite the boundary conditions of problem (1.2):

$$\varphi_0'(t) + \bar{t}\varphi_1'(t) + \varphi_1(t) = -[\overline{\varphi_0'(t)} + \overline{t\varphi_1'(t)} + \overline{\varphi_1(t)}] + 2c_1(t), \quad (1.4)$$

$$\varphi_0'(t) + \bar{t}\varphi_1'(t) - \varphi_1(t) = -[\overline{\varphi_0'(t)} + \overline{t\varphi_1'(t)} - \overline{\varphi_1(t)}] - 2ic_2(t). \quad (1.5)$$

Using notation

$$\Phi(z) = \varphi_0'(z), \quad Q_1(z) = -\bar{t}\varphi_1'(t) - \varphi_1(t) - \overline{t\varphi_1'(t)} - \overline{\varphi_1(t)} + 2c_1(t), \quad (1.6)$$

we can rewrite the boundary condition of (1.4) as

$$\Phi_0(t) = -\overline{\Phi_0(t)} + Q_1(t). \quad (1.7)$$

In the case of circle K_1 the kernel

$$K(t, \tau) = \frac{1}{2\pi i} \left[\frac{1}{\tau - t} - \frac{[\tau'(\sigma)]^2}{\bar{\tau} - \bar{t}} \right]$$

of the integral equation

$$\mu_0(t) + \frac{1}{2\pi i} \int_L K(t, \tau) \mu_0(\tau) d\tau = Q_1(t)$$

is defined by the formula

$$K(t, \tau) = \frac{1}{2\pi i} \frac{1}{\tau},$$

and its resolvent $R_{10}(t, \tau) = -4\pi i/\tau$.

Considering temporarily $Q_1(\tau)$ as the known function and solving the Gilbert boundary value problem (1.7) with the coefficient $G_1(t) = -1$ we obtain

$$\Phi_0(z) = \frac{1}{2\pi i} \int_{\gamma_1} \frac{Q_1(\tau)}{\tau - z} d\tau - \frac{1}{4\pi i} \int_{\gamma_1} \frac{Q_1(\tau)}{\tau} d\tau + i\epsilon_0, \quad (1.8)$$

where ϵ_0 is an arbitrary real constant.

Substituting in (1.8) for $Q_1(\tau)$ its value from (1.6) we obtain

$$\begin{aligned} \Phi_0(z) = & -\frac{\varphi_1'(z)}{z} - \varphi_1(z) + \frac{\varphi_1'(0)}{z} - \overline{z\varphi_1'(0)} + iIm\varphi_1(0) + iIm\varphi_1''(0) \\ & + \frac{1}{\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau - z} d\tau - \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau} d\tau + i\epsilon_0. \end{aligned} \quad (1.9)$$

Passing on to the limit by $z \rightarrow t \in \gamma_1$ and taking into consideration (1.3) we obtain from (1.9) that

$$\begin{aligned} \Phi_0(t) = & -\bar{t}\varphi_1'(t) - \varphi_1(t) - 2iIm\{\overline{t\varphi_1'(0)}\} + iIm\varphi_1''(0) \\ & + c_1(t) + \frac{1}{\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau - t} d\tau - \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau} d\tau + i\epsilon_0, \end{aligned} \quad (1.10)$$

$$\begin{aligned} \overline{\Phi_0(t)} = & -\overline{t\varphi_1'(t)} - \overline{\varphi_1(t)} - 2iIm\{\overline{t\varphi_1'(0)}\} + iIm\varphi_1''(0) \\ & + c_1(t) - \frac{1}{\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau - t} d\tau + \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau} d\tau - i\epsilon_0. \end{aligned} \quad (1.11)$$

Substituting in (1.5) for $\varphi_0'(t) = \Phi_0(t)$ and $\overline{\varphi_0'(t)} = \overline{\Phi_0(t)}$ their values from (1.10) and (1.11) we get

$$\phi_1(t) = \overline{\phi_1(t)} + Q_2(t), \quad (1.12)$$

where

$$\begin{aligned} Q_2(t) = & \frac{1}{\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau - t} d\tau - \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau} d\tau + ic_2(t) \\ & + 2iIm\{\bar{t}\varphi_1'(0)\} + iIm\{\bar{t}\varphi_1''(0)\} + i\epsilon_0. \end{aligned} \quad (1.13)$$

Considering temporarily $Q_2(t)$ as the known function and solving the Gilbert boundary value problem (1.12) with the coefficient $G_2(t) = 1$, we obtain

$$\varphi_1(z) = \frac{1}{2\pi i} \int_{\gamma_1} \frac{Q_2(\tau)}{\tau - z} d\tau - \frac{1}{4\pi i} \int_{\gamma_1} \frac{Q_2(\tau)}{\tau} d\tau + \epsilon_1, \quad (1.14)$$

where ϵ_1 is an arbitrary real constant.

Substituting in the right-hand side of (1.14) for $Q_2(t)$ its value from (1.13), we get the equality

$$\begin{aligned} \varphi_1(z) = & \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau - z} d\tau - \frac{1}{4\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau} d\tau \\ & - \frac{1}{4\pi i} \int_{\gamma_1} \frac{c_1(\tau)}{\tau} d\tau + \frac{i}{2} \text{Im} \varphi_0''(0) + \frac{i}{2} \epsilon_0 + \epsilon_1 - z \overline{\varphi_0'(z)}. \end{aligned} \quad (1.15)$$

Taking into account that $\varphi_1(0) = 0$ and setting $z = 0$ from (1.15) we obtain

$$0 = \frac{1}{4\pi i} \int_{\gamma_1} \frac{ic_2(t)}{\tau} d\tau + \frac{i}{2} \epsilon_0 + \epsilon_1.$$

But the last equation is equivalent to the system

$$\begin{cases} l\epsilon_1 = 0, \\ \epsilon_0 = -\text{Im} \varphi_1''(0) - \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_2(\tau)}{\tau} d\tau. \end{cases} \quad (1.16)$$

Taking into consideration (1.16) we can obtain from (1.15)

$$\varphi_1(z) = -\frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau - z} d\tau - \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau} d\tau - z \overline{\varphi_0'(0)}. \quad (1.17)$$

Differentiating equation (1.17) we have

$$\varphi_1'(z) = \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{(\tau - z)^2} d\tau - \overline{\varphi_1'(0)}. \quad (1.18)$$

Substituting in (1.18) $z = 0$ we obtain

$$\varphi_1'(0) + \overline{\varphi_1'(0)} = \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau. \quad (1.19)$$

But equation (1.19) can take place if and only if

$$\text{Im} \left\{ \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau \right\} = 0. \quad (1.20)$$

Let us permit that condition (1.20) is fulfilled. Then, from (1.17), (1.18), taking into consideration (1.19) and the equation $Im\varphi_1'(0) = 0$ we obtain

$$\begin{aligned} \varphi_1(z) = & \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau - z} d\tau \\ & - \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau} d\tau - \frac{z}{4\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau, \end{aligned} \quad (1.21)$$

$$\varphi_1'(z) = \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{(\tau - z)^2} d\tau - \frac{1}{4\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau. \quad (1.22)$$

Since $c_1(t), c_2(t) \in H^{(1)}(\gamma_1)$ we can rewrite the formula (1.22) as:

$$\begin{aligned} \varphi_1'(z) = & \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1'(\tau) - ic_2'(\tau)}{\tau - z} d\tau \\ & - \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{(\tau - z)^2} d\tau + \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau. \end{aligned}$$

Then substituting in $Q_1(\tau)$ of the boundary condition (1.7) for $\varphi_1(t), \overline{\varphi_1(t)}, \varphi_1'(t), \overline{\varphi_1'(t)}$ the boundary values of functions found by formulae (1.21) and (1.22) $\varphi_1(z), \varphi_1'(z)$ and solving the boundary value problem (1.7) we have

$$\begin{aligned} \Phi_0(z) = & \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) - ic_2(\tau)}{\tau - z} d\tau + \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{(\tau - z)^2} d\tau \\ & + \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau. \end{aligned}$$

Then with the help of integration and taking into consideration (1.3) we have

$$\begin{aligned} \phi_0(z) = & \int_{\Gamma} \left\{ \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) - ic_2(\tau)}{\tau - z} d\tau + \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{(\tau - z)^2} d\tau \right. \\ & \left. + \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau \right\} dz + \delta_0, \end{aligned} \quad (1.23)$$

where Γ is an arbitrary smooth curve, belonging to circle K_1 and connecting points 0 and z , and δ_0 is an arbitrary real constant. Then we can determine

function $F(z)$ by the formula

$$F(z) = \varphi_0(z) + \bar{z}\varphi_1(z),$$

where $\varphi_0(z)$ and $\varphi_1(z)$ are determined by formulae (1.23) and (1.21), respectively. This result was published in [3].

2. A METHOD FOR OBTAINING THE EQUATION OF THE BEND OF THE ROUND FIXED PLATE UNDER THE LOADING

Let us apply this result to the solution of the following problem: find the equation of the bend of the round fixed plate under the concentrated loading P , applied at the point $M_0(z_0)$.

It is known, that the equation of the bend of such a plate has a form

$$w = w(z),$$

where $w(x, y)$ satisfies the differential equation

$$\Delta^2 w = \frac{P}{D} \delta(z - z_0). \quad (2.1)$$

Here D is the rigidity of the plate with the flexure, $\delta(z)$ is the Dirac function, and also the following boundary conditions are fulfilled for the function $w(x, y)$

$$w|_{|z|=1} = 0; \quad \frac{\partial w}{\partial x}|_{|z|=1} = 0; \quad \frac{\partial w}{\partial y}|_{|z|=1} = 0.$$

We search for the solution of the equation (31) in the form

$$w = \tilde{u} + w_0,$$

where $\tilde{u}(x, y)$ is a byharmonic function,

$$w_0 = \frac{P}{16\pi D} (z - z_0)(\bar{z} - \bar{z}_0) \cdot \ln((z - z_0)(\bar{z} - \bar{z}_0)). \quad (2.2)$$

Function $w_0(z)$ is a special solution of the equation (2.1) (see [2], p. 379). Then function $u(x, y) = \frac{16\pi D}{P} \tilde{u}(x, y)$ satisfies the following boundary conditions

$$\begin{aligned} c_1(t)|_{|t|=1} &= \frac{\partial u}{\partial x}|_{|t|=1} = -2\operatorname{Re}[(t - z_0)(1 + \ln((t - z_0)(\bar{t} - \bar{z}_0)))] \\ c_2(t)|_{|t|=1} &= \frac{\partial u}{\partial y}|_{|t|=1} = -2\operatorname{Im}[(t - z_0)(1 + \ln((t - z_0)(\bar{t} - \bar{z}_0)))] \end{aligned}$$

Let us compute the integral

$$\frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) + ic_2(t)}{t - z} dt.$$

Substituting their values of $c_1(t)$ and $c_2(t)$ from (2.2), we obtain

$$\begin{aligned} & -2 \frac{1}{2\pi i} \int_{\gamma_1} \frac{(t - z_0)(1 + \ln(t - z)(\bar{t} - \bar{z}_0))}{t - z} dt \\ & = 2 \frac{1}{2\pi i} \int_{\gamma_1} \frac{(t - z_0)(1 + \ln(t - z)(\frac{1}{t} - \bar{z}_0))}{t - z} dt \\ & = 2 \frac{1}{2\pi i} \int_{\gamma_1} \frac{(t - z_0)(1 + \ln(1 - t\bar{z}_0) \cdot \ln(1 - \frac{z_0}{t}))}{t - z} dt \\ & = -2 \left[\frac{1}{2\pi i} \int_{\gamma_1} \frac{(t - z_0)(1 + \ln(1 - t\bar{z}_0))}{t - z} dt \right. \\ & \quad \left. + \frac{1}{2\pi i} \int_{\gamma_1} \frac{(t - z_0) \left(\frac{z_0}{t} + \frac{z_0^2}{2t^2} + \dots \right)}{t - z} dt \right]. \end{aligned}$$

The first integral, as the integral from function, analytic in the circle K_1 , is equal to

$$(z - z_0)(1 + \ln(1 - z \cdot \bar{z}_0)).$$

We compute the second integral, applying the theorem about the residues. It is equal to z_0 . Consequently,

$$\frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) + ic_2(t)}{t - z} dt = -2[(z - z_0)(1 + \ln(1 - \bar{z}_0 \cdot z) + z_0)].$$

Hence we easily obtain

$$\begin{aligned} \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) + ic_2(t)}{(t - z)^2} dt &= -2 \left[1 - \frac{\bar{z}_0(z - z_0)}{1 - \bar{z}_0 \cdot z} + \ln(1 - \bar{z}_0 \cdot z) \right], \\ \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) + ic_2(t)}{t} dt &= 0, \\ \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) + ic_2(t)}{t^2} dt &= -2(1 + |z_0|^2). \end{aligned}$$

Let us compute the integral

$$\frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) - ic_2(t)}{t - z} dt.$$

Substituting the values of $c_1(t)$ and $c_2(t)$, we obtain

$$\begin{aligned} & -2 \cdot \frac{1}{2\pi i} \int_{\gamma_1} \frac{(\bar{t} - \bar{z}_0)(1 + \ln((\bar{t} - \bar{z}_0)(t - z_0)))}{t - z} dt \\ &= -2 \cdot \frac{1}{2\pi i} \int_{\gamma_1} \frac{\left(\frac{1}{t} - \bar{z}_0\right) \left(1 + \ln\left(\left(1 - \frac{z_0}{t}\right) \cdot (1 - t \cdot \bar{z}_0)\right)\right)}{t - z} dt \\ &= -2 \cdot \frac{1}{2\pi i} \int_{\gamma_1} \frac{\left(\frac{1}{t} - \bar{z}_0\right) \left(1 + \ln(1 - t\bar{z}_0) + \frac{z_0}{t} + \frac{z_0^2}{2t^2} + \dots\right)}{t - z} dt. \end{aligned}$$

Applying the theorem about the residues, we obtain

$$\frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) - ic_2(t)}{t - z} dt = -2 \left[\bar{z}_0 + \left(-\bar{z}_0 + \frac{1}{z}\right) \ln(1 - \bar{z}_0 z) \right].$$

Now let us find the function

$$\begin{aligned} \varphi_1(z) &= \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau - z} d\tau - \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau} d\tau \\ &\quad - \frac{z}{4\pi i} \int_{\gamma_1} \frac{c_1(\tau) + ic_2(\tau)}{\tau^2} d\tau \\ &= -2 \left[z_0 + (z - \bar{z}_0) \left(1 + \ln(1 - z\bar{z}_0) - \frac{z(1 + |z_0|^2)}{2}\right) \right] \\ &= z - |z_0|^2 z - 2z \ln(1 - z\bar{z}_0) + 2z_0 \ln(1 - z\bar{z}_0). \end{aligned}$$

After the elementary transformations we obtain

$$\begin{aligned} & \frac{1}{2\pi i} \int_{\gamma_1} \frac{c_1(t) - ic_2(t)}{t - z} dt - \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(t) + ic_2(t)}{(t - z)^2} dt + \frac{z^{-1}}{2\pi i} \int_{\gamma_1} \frac{c_1(t) + ic_2(t)}{t^2} dt \\ &= -2 \left(\frac{\bar{z}_0^2 \cdot z - \bar{z}_0^2 \cdot z_0}{1 - \bar{z}_0 \cdot z} - \bar{z}_0 \ln(1 - \bar{z}_0 \cdot z) \right). \quad (2.3) \end{aligned}$$

It follows from (2.3), that

$$\varphi_0(z) = 2(\bar{z}_0 z \ln(1 - \bar{z}_0 z) - |z_0|^2 \ln(1 - \bar{z}_0 z)) + 1 - |z_0|^2.$$

Hence

$$\begin{aligned} \varphi_0(z) + \bar{z}\varphi_1(z) &= 2(\bar{z}_0 z \cdot \ln(1 - \bar{z}_0 z) - |z_0|^2 \ln(1 - \bar{z}_0 z)) + 1 - z^2 \\ &\quad + \bar{z}(-z + z_0^2 z - 2(z - z_0) \ln(1 - \bar{z}_0 z)) \\ &= (1 - |z_0|^2)(1 - |z|^2 - |z - z_0|^2 \ln(1 - \bar{z}_0 z)^2). \end{aligned}$$

Consequently

$$u(x, y) = \operatorname{Re}(\varphi_0(z) + \bar{z}\varphi_1(z)) = (1 + |z_0|^2)(1 - |z|^2) - |z - z_0|^2 \ln(1 - \bar{z}_0 z)^2.$$

Hence the equation of the blend of the plate has a form

$$w(x, y) = \frac{P}{16\pi D} \left[(1 - |z_0|^2)(1 - |z|^2) \right] + \ln \left| \frac{z - z_0}{1 - \bar{z}_0 z} \right|^2.$$

In order to obtain the equation of the round fixed plate of radius r we must substitute in (2.1) $\frac{z}{r}$ for z and $\frac{z_0}{r}$ for z_0 . Another proof of this result can be found in [5]. Let us find the equation of the blend of the fixed round plate of radius 1, if the loading is concentrated on the interior circumference γ with the intensity P . The case of circumference γ , which is concentric with the plate, was considered in [4]. Let us use the Cartesian coordinate system and suppose that the center of the plate coincides with the beginning of coordinates, and the center of circumference γ is the point with the complex coordinate u .

It was proved in [4], that if the loading is concentrated at the point z_0 , the equation of the blend of the surface has a form

$$w(z) = \frac{P}{16\pi D} \left[(1 - |z_0|^2)(1 - |z|^2) - |z - z_0|^2 \ln \left| \frac{z - z_0}{1 - \bar{z}_0 z} \right|^2 \right].$$

Hence, if t is a point of the circumference γ , the equation of the blend of the plate has a form

$$w(z) = \frac{P}{16\pi D} \int_{\gamma} \left[(1 - |t|^2)(1 - |z|^2) + |z - t|^2 \ln \left| \frac{z - t}{1 - \bar{t}z} \right|^2 \right] dl,$$

where dl is an element of the length of the arc γ . Let us compute the integral

$$I_1 = \int_{\gamma} [(1 - |t|^2)(1 - |z|^2)] dl.$$

We rewrite an element of the arc dl in the form

$$dl = rd\varphi = \frac{ir^2 e^{i\varphi} d\varphi}{ire^{i\varphi}} = \frac{rd(t-u)}{i(t-u)} = \frac{irdt}{t-u}.$$

Due to equality $(t-u)(\bar{t}-\bar{u}) = r^2$ we have $\bar{t} = \frac{r^2}{t-u} + \bar{u}$. Hence

$$\begin{aligned} I_1 &= \int_{\gamma} [(1-|t|^2)(1-|z|^2)] dl \\ &= -(1-|z|^2) \int_{\gamma} \frac{ir}{t-u} [1-t(\frac{r^2}{t-u} + u)] dt. \end{aligned}$$

Applying the theorem about the residues (see [2]), we obtain

$$I_1 = 2\pi r (1-r^2-u^2) (1-|z|^2).$$

Now let us find the integral $\int_{\gamma} |t-z|^2 \ln |t-z|^2 dl$. Firstly, we suppose that $|z-u| < r$. Then

$$\begin{aligned} |t-z|^2 &= |(t-u) - (z-u)|^2 = [(t-u) - (z-u)][(\bar{t}-\bar{u}) - (\bar{z}-\bar{u})] \\ &= (t-u)(\bar{t}-\bar{u}) \left(1 - \frac{z-u}{t-u}\right) \left(1 - \frac{\bar{z}-\bar{u}}{\bar{t}-\bar{u}}\right) \\ &= r^2 \left(1 - \frac{z-u}{t-u}\right) \left(1 - \frac{(\bar{z}-\bar{u})(t-u)}{r^2}\right). \end{aligned}$$

Hence

$$\begin{aligned} I_{21} &= \int_{\gamma} |t-z|^2 \ln |t-z|^2 dl \\ &= \int_{\gamma} |t-z|^2 \ln \left[r^2 \left(1 - \frac{z-u}{t-u}\right) \left(1 - \frac{\bar{z}-\bar{u}}{\bar{t}-\bar{u}}\right) \right] dl \\ &= \ln r^2 \int_{\gamma} |t-z|^2 dl + 2Re \int_{\gamma} |t-z|^2 \ln \left(1 - \frac{(\bar{z}-\bar{u})(t-u)}{r^2}\right) dl \\ &= r^2 \ln r^2 \int_{\gamma} \left(1 - \frac{z-u}{t-u}\right) \left(1 - \frac{(\bar{z}-\bar{u})(t-u)}{r^2}\right) \frac{-ir}{t-u} dt \\ &\quad + 2r^2 Re \int_{\gamma} \left(1 - \frac{z-u}{t-u}\right) \left[1 - \frac{(\bar{z}-\bar{u})(t-u)}{r^2}\right] \ln \left(1 - \frac{(\bar{z}-\bar{u})(t-u)}{r^2}\right) \frac{irdt}{t-u}. \end{aligned}$$

Applying the theorem about the residues, we obtain the equality

$$I_{21} = 2\pi r \ln r (r^2 + |z - u|^2) + 4\pi r |z - u|^2.$$

Now let us suppose that $|z - u| > r$. Then

$$\begin{aligned} |z - t|^2 &= [(z - u) - (t - u)][(\bar{z} - \bar{u}) - (\bar{t} - \bar{u})] \\ &= (z - u)(\bar{z} - \bar{u}) \left(1 - \frac{1 - u}{z - u}\right) \left(1 - \frac{\bar{t} - \bar{u}}{z - u}\right) \\ &= |z - u|^2 \left(1 - \frac{1 - u}{z - u}\right) \left(1 - \frac{r^2}{(z - u)(t - u)}\right). \end{aligned}$$

Thus we have proved that $I_{31} = I_{32} = I_3$.

3. MAIN FORMULA

We have proved that the equation of the blend of the plate has a form

$$\begin{aligned} w &= \frac{P}{16\pi D} \left[2\pi r (1 - r^2 - |u|^2) (1 - |z|^2) + 2\pi r \ln r^2 (r^2 + |z - u|^2) \right. \\ &\quad \left. + 4\pi r |z - u|^2 - 2\pi r (r^2 + |z - u|^2) \ln |1 - u\bar{z}|^2 - 4\pi r^3 \operatorname{Re} \frac{\bar{z}(z - u)}{1 - \bar{z}u} \right], \end{aligned}$$

if $|z - u| < r$, and

$$\begin{aligned} w &= \frac{P}{16\pi D} \left[2\pi r (1 - r^2 - |u|^2) (1 - |z|^2) + 2\pi r \ln |z - u|^2 (r^2 + |z - u|^2) \right. \\ &\quad \left. + 4\pi r^3 - 2\pi r (r^2 + |z - u|^2) \ln |1 - u\bar{z}|^2 - 4\pi r^3 \operatorname{Re} \frac{\bar{z}(z - u)}{1 - \bar{z}u} \right], \end{aligned}$$

if $|z - u| > r$.

Let assume that the loading P is a real valued function of the coordinates $P = P(x, y)$.

We denote

$$P_1(x, y) = -\frac{\partial w_0}{\partial x} \frac{1}{D}, \quad P_2(x, y) = -\frac{\partial w_0}{\partial y} \frac{1}{D},$$

where D is a cylindrical rigidity of the plate. Then on the unit circumference

$$\begin{aligned} P_1(x, y) &= P_1\left(\frac{t + \bar{t}}{2}, \frac{t - \bar{t}}{2i}\right) = P_1\left(\frac{t + \frac{1}{\bar{t}}}{2}, \frac{t - \frac{1}{\bar{t}}}{2i}\right) = c_1(t), \\ P_2(x, y) &= P_2\left(\frac{t + \bar{t}}{2}, \frac{t - \bar{t}}{2i}\right) = P_2\left(\frac{t + \frac{1}{\bar{t}}}{2}, \frac{t - \frac{1}{\bar{t}}}{2i}\right) = c_2(t), \end{aligned}$$

where $|t| = 1$. In this case for computation of the integrals in (1.21) and (1.23) we can use the theorem about residues.

Let the loading $q(x, y)$ be an arbitrary twice continuously differentiable function of coordinates. Then for computation of integrals in (1.21) and (1.23) we can use the approximate method, described in our article [3].

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Apie vieno uždavinio elastiškumo teorijoje sprendimo metodą

V.R. Kristalinskii

Straipsnyje kompleksinio kintamojo analizės ir kompiuterinės algebros metodai taikomi sprendžiant eilę uždavinių, kurių tikslas surasti apskrities įtvirtintos plokštelės lygtis, kai ją veikia įvairaus tipo apkrovos. Gauti rezultatai testuojami pavyzdžiais. Gauta keletas naujų rezultatų. Išnagrinėtas atvejis, kai apkrovos pasiskirsčiusios nekoncentriškais apskritimais, atkarpa arba laisvai bet koku būdu visoje plokštelėje.